

# SPECIFICATION

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## ALUMINIDE COATING PROCESS

### Background of Invention

#### Field of the Invention

[0001] The present invention relates to processes for forming aluminide coatings. More particularly, this invention relates to a process of forming an aluminide coating on a surface of a component having an existing thermal barrier coating without causing spallation of the thermal barrier coating.

#### Description of the Related Art

[0002] The operating environment within a gas turbine engine is both thermally and chemically hostile. Significant advances in high temperature capabilities have been achieved through the development of iron, nickel and cobalt-base superalloys and the use of oxidation-resistant environmental coatings capable of protecting superalloys from oxidation, hot corrosion, etc. Aluminum-containing coatings, particularly diffusion aluminide coatings, have found widespread use as environmental coatings on gas turbine engine components. Aluminide coatings are generally formed by a diffusion process such as pack cementation or vapor phase aluminizing (VPA) techniques, or by diffusing aluminum deposited by chemical vapor deposition (CVD) or slurry coating. During high temperature exposure in air, an aluminide coating forms a protective aluminum oxide (alumina) scale or layer that inhibits oxidation of the coating and the underlying substrate.

[0003] Slurry coatings used to form aluminide coatings contain an aluminum powder in an inorganic binder, and are directly applied to the surface to be aluminized. Aluminizing occurs as a result of heating the component in a non-oxidizing atmosphere or vacuum to a temperature that is maintained for a duration sufficient to melt the aluminum powder and diffuse the molten aluminum into the surface. As

described in U.S. Patent No. 6,444,054, slurry coatings may contain a carrier (activator), such as an alkali metal halide, which vaporizes and reacts with the aluminum powder to form a volatile aluminum halide, which then reacts at the component surface to form the aluminide coating. Because the thickness of an aluminide coating produced by a slurry method is proportional to the amount of the slurry applied to the surface, the amount of slurry applied must be very carefully controlled. While the presence of a halide is believed to displace oxides on the surface being treated, making it more likely that a clean uniform diffusion coating will result, the inability of slurry processes to consistently produce diffusion aluminide coatings of uniform thickness has discouraged their use on components that require a very uniform diffusion coating and/or have complicated geometries, such as turbine blades.

[0004] In contrast to slurry processes, pack cementation and VPA processes are widely used to form aluminide coatings because of their ability to form coatings of uniform thickness. Both of these processes generally entail reacting the surface of a component with an aluminum halide gas formed by reacting an activator (e.g., an ammonium or alkali metal halide) with an aluminum-containing source (donor) material. In pack cementation processes, the aluminum halide gas is produced by heating a powder mixture comprising the source material, the activator, and an inert filler such as calcined alumina. The ingredients of the powder mixture are mixed and then packed and pressed around the component to be treated, after which the component and powder mixture are heated to a temperature sufficient to vaporize the activator, which reacts with the source material to form the volatile aluminum halide, which then reacts at the component surface to form the aluminide coating. In contrast to pack processes, VPA processes are carried out with the source material placed out of contact with the surface to be aluminized. The source material can be an aluminum alloy or an aluminum halide, the latter of which eliminates the requirement for a separate activator. Aside from certain limited exceptions, such as a pack cementation process taught by U.S. Patent No. 5,254,413 to Maricocchi and a VPA process taught by 6,326,057 to Das et al., both of which are assigned to the assignee of this invention, all conventional pack cementation and VPA processes have required the use of halide carriers or activators.



formed before any external coatings are applied, the final configuration of the hole opening is difficult to maintain and measure. For example, thermally-sprayed bond coats are typically deposited in one or more applications having tolerances that may be on the order of about 20% to 30%. TBC's applied by some form of thermal spray process, such as plasma spraying, high velocity oxy-fuel (HVOF), etc., are also inherently difficult to control on a local scale. As a result, the precise size and shape of a film cooling hole and other small, well-defined, features present in a component surface are lost, blurred, or otherwise altered by the subsequent deposition of a protective coating. On the other hand, processing complications are encountered if cooling holes are formed after the deposition of a protective coating. For example, bond coats are formed of hard, brittle materials that are very difficult to machine. Furthermore, the aluminide coatings desired for the internal cooling passages cannot be deposited after TBC deposition because the halide activator required by aluminide coating processes traditionally suitable for gas turbine components are incompatible with TBC materials. A TBC exposed during such an aluminizing process de-bonds or spalls from the component, leaving the area underneath with little or no thermal protection. Consequently, gas turbine engine components requiring both air cooling and TBC for thermal protection have been designed so that their cooling holes are properly sized after bond coat and TBC deposition, or their holes must be reopened after TBC deposition with the risk of damage to the aluminide coating protecting the cooling hole. Such damage to the internal aluminide coating is virtually impossible to detect and can lead to premature failure of the component.

[0008]

In view of the above, it can be appreciated that the ability to combine cooling air flow, TBC, and aluminized cooling holes in the same component has not been fully realized because aluminized cooling holes are prone to damage when attempting to reestablish their shape and size after bond coat and TBC deposition, and the aluminizing of cooling holes after bond coat and TBC deposition is prohibited by the reaction that occurs between the halide and TBC. As a result of the latter, virtually all TBC-coated air-cooled gas turbine engine components equipped with film cooling holes have been manufactured according to the following sequence: machine the cooling holes; aluminide coat the cooling holes; and then deposit the TBC over the pre-machined, pre-coated, cooling holes, with the result that the cooling holes are at

least partially blocked with TBC. It is believed that all prior attempts to rearrange the manufacturing sequence so that cooling hole machining and internal aluminide coating are performed after TBC deposition have failed because of the incompatibility of the halide activator and TBC materials.

[0009] Because TBC's are frangible, TBC-coated components are at risk of damage from handling that can lead to the loss of thermal protection, resulting in a local increase in component temperature during engine operation that may be unacceptable if the chipped region is sufficiently large. In this case, the TBC must typically be stripped from the entire component and reapplied. If the component is air-cooled, the reapplied TBC must be removed from the cooling holes in order to reestablish their size and geometry. As previously discussed, any aluminide coating present within a cooling hole that must undergo refurbishment in this manner is prone to damage and even removal when attempting to remove the TBC blocking the hole. Therefore, in addition to the desirability of combining different forms of thermal protection, it would be advantageous if, during the repair of a TBC-coated component, the oxidation resistance of the exposed bond coat could be enhanced by local application of an aluminide, instead of completely stripping and recoating the entire component. Furthermore, it would be advantageous if a component having TBC applied to only limited external surfaces (whether intentional or not) could be aluminized after TBC deposition to provide environmental protection on those surfaces not covered by the TBC. However, each of these capabilities has also been frustrated by the incompatibility between TBC and the halide activators used in aluminizing processes.

## Summary of Invention

[0010] The present invention is an aluminiding process that enables the cooling holes of an air-cooled component, such as a hot gas path component of a gas turbine engine, to be machined and aluminized after all other surface coatings have been deposited. This sequence eliminates the previous requirement to machine the cooling holes before any coatings are applied, which resulted in the size and shape of the cooling holes, and hence the cooling flow characteristics of the component, being undesirably altered by the deposited coatings.

[0011] The invention is generally a slurry process for forming an aluminide coating.

According to this invention, the process is able to form a diffusion aluminide coating on a component having a ceramic coating on a first surface thereof, without damaging the ceramic coating. The process involves applying an activator-free slurry on a second surface of the component that is not covered by the ceramic coating. The slurry contains aluminum particles that, when the component is heated in an inert or reducing atmosphere, melt and the resulting molten aluminum diffuses into the second surface of the component, thereby forming the desired diffusion aluminide coating on the second surface.

[0012] In view of the above, the process of this invention is able to produce a diffusion aluminide coating without the use of a halide carrier or activator. As a result, the process can be employed to aluminize the internal surfaces of cooling holes of an air-cooled component after deposition of a TBC required to thermally protect the external surfaces of the component. The invention is also useful in other circumstances where it is desirable to aluminize a surface of a component having an existing TBC, such as when repairing or refurbishing a diffusion bond coat exposed by a spalled region of TBC.

[0013] Other objects and advantages of this invention will be better appreciated from the following detailed description.

## Brief Description of Drawings

[0014] Figures 1, 2 and 3 represent partial cross-sectional views of an air-cooled component having a TBC on an external surface thereof, and illustrates the steps of machining a cooling hole in the component (Figure 2) and then aluminiding the internal surface of the hole without spalling the TBC on the external surface (Figure 3) in accordance with this invention.

## Detailed Description

[0015] The present invention is generally applicable to components that operate within thermally and chemically hostile environments, and are therefore subjected to oxidation, hot corrosion and thermal degradation. Examples of such components include the high and low pressure turbine nozzles, blades and shrouds of gas turbine engines. While the advantages of this invention will be described with reference to gas

turbine engine hardware, the teachings of the invention are generally applicable to any component on which both an aluminide coating and a TBC are used to protect the component from its hostile operating environment.

[0016] Figure 1 represents a partial cross-section of a gas turbine engine component 10, such as a turbine blade, whose external surface 18 is protected by a thermal barrier coating (TBC) system 12. The TBC system 12 is shown as including a bond coat 14 on which a ceramic TBC 16 is deposited. Typical materials for the component 10 include nickel, iron and cobalt-base superalloys, though other alloys could be used. The TBC 16 may be deposited by thermal spraying such as air plasma spraying (APS), low pressure plasma spraying (LPPS) and HVOF, or by a physical vapor deposition technique such as electron beam physical vapor deposition (EBPVD). A preferred material for the TBC 16 is zirconia partially stabilized with yttria (yttria-stabilized zirconia, or YSZ), though zirconia fully stabilized with yttria could be used, as well as zirconia stabilized by other oxides, such as magnesia (MgO), calcia (CaO), ceria ( $\text{CeO}_2$ ) or scandia ( $\text{Sc}_2\text{O}_3$ ). The bond coat 14 serves to adhere the ceramic TBC 16, and will typically be a thermal-sprayed overlay coating (e.g., MCrAlY) if the TBC 16 is deposited by thermal spraying, or a diffusion aluminide if the TBC 16 is deposited by PVD. When sufficiently heated in an oxidizing atmosphere, the coating 14 develops an alumina ( $\text{Al}_2\text{O}_3$ ) layer or scale (not shown) on its surface that protects the underlying superalloy surface 18 from oxidation.

[0017] According to this invention, the component 10 is desired to be film air-cooled, requiring the creation of cooling holes between the component surface 18 and an internal passage 20 within the component 10. A representative cooling hole 22 is depicted in Figure 2, and is shown as having been machined by any suitable technique through the wall of the component 10 defined between the external surface 18 and internal passage 20. To protect the internal surface 24 defined by the hole 22, a diffusion aluminide coating 26 (Figure 3) is formed by a slurry process by which aluminum is diffused into the surface 24 to form aluminide intermetallics. As with conventional diffusion aluminide coatings, the aluminide coating 26 of this invention is characterized by two distinct zones (not shown), namely, an outermost additive layer containing MAI intermetallic compounds and a diffusion zone beneath the additive layer and comprising various intermetallic and metastable phases.





commercially known as GTD-111 and having a nominal composition, in weight percent, of Ni-14.0Cr-9.5Co-3.0Al-4.9Ti-1.5Mo-3.8W-2.8Ta-0.010C. Each button had one surface coated with a TBC system comprising an MCrAlY bond coat (where M is nickel, cobalt and/or iron) deposited by LPPS (also referred to as vacuum plasma spraying (VPS)), on which a TBC top coat of zirconia stabilized by about 4 to 8 weight percent yttria was deposited by air plasma spraying (APS) to a thickness of about 0.012 inch (about 0.3 mm). Six of the twelve buttons were set aside as baseline specimens, while the remaining six buttons were completely coated with the SermAlcote slurry to a thickness of about 0.020 to 0.080 inch (about 0.5 to about 2 mm). After drying the slurry coatings at room temperature overnight, the six slurry-coated buttons underwent currying at about 600 ° F (about 320 ° C) for about thirty minutes, followed by a diffusion heat treatment at a temperature of about 1950 ° F (about 1065 ° C) for a duration of about two hours in an evacuated retort, resulting in the six buttons developing diffusion aluminide coatings on those surfaces free of the TBC. Residual aluminum was not observed on the TBC on which the slurry had been deposited.

[0021] All twelve buttons were then subjected to thermal cycle testing. Three of the aluminized buttons and three baseline buttons were cycled between room temperature and about 2000 ° F (about 1090 ° C) with a forty-five minute soak at the elevated temperature, while the remaining three aluminized buttons and three baseline buttons were cycled between room temperature and about 2000 ° F (about 1090 ° C) with a twenty-hour soak at the elevated temperature. All buttons were cycled until about 10 percent of the surface area of the TBC had spalled. Results of the thermal cycle tests are summarized in Table I below.

[t1]

Table I

	Cycles to Spallation	Cycles to Spallation
Specimen	2000 ° F/45 min hold	2000 ° F/20 hr hold
Baseline	440	29
	560	45

	869	35
Slurry-coated	600	20
	620	45
	620	55

[0022] From this investigation, it can be seen that no significant difference in spallation resistance was apparent between the baseline and aluminized buttons. It was therefore concluded that the slurry process is capable of producing a diffusion aluminide coating on a surface of a substrate without damaging an existing TBC on the same substrate.

[0023] While the invention has been described in terms of a preferred embodiment, it is apparent that other forms could be adopted by one skilled in the art. Accordingly, the scope of the invention is to be limited only by the following claims.